Comparing Castability of Nickel-Chromium, Cobalt-Chromium, and Non-Precious Gold Color Alloys, Using two Different Casting Techniques

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ABSTRACT

Statement of the Problem: The castability of nonprecious gold color alloy using torch/centrifugal and induction/vacuum-pressure casting techniques has not been studied yet.

Purpose: This study was conducted to compare the castability of nickel chromium, cobalt-chromium and nonprecious gold color alloy using torch/centrifugal and induction/ vacuum-pressure casting techniques.

Materials and Method: In this in vitro study, a total number of 54 identical acrylic wax meshes were prepared and divided into 6 different groups of 9 each. Group 1: nickel-chromium alloy, which was casted with induction technique. Group 2: nickel-chromium alloy was casted with centrifugal technique. Group 3: cobalt-chromium alloy was casted with induction technique. Group 4: cobalt-chromium alloy was casted with centrifugal technique. Group 5: nonprecious gold color alloy was casted with induction technique. Group 6: nonprecious gold color alloy was casted with centrifugal technique. Then castability of specimens was measured using modified Whitlock’s method. The results were analyzed using two way ANOVA and post hoc tests.

Results: ANOVA test revealed no statistically significant difference between different alloys with a p Value of 0.313. Moreover, it represented no significant differences within the groups regarding alloy types and casting techniques with a p Value of 0.511 and 0.682, respectively.

Conclusion: No significant difference was found in the castability value of nickel-chromium, cobalt-chromium, and nonprecious gold color alloys. In addition, the castability value of three alloys tested in this study was not different by using torch/centrifugal or induction/vacuum-pressure casting machines.

than Ni-Cr. The casting process of Co-Cr is convenient and it is cost benefit. Co-Cr alloy can be used for metal ceramic restorations; the bond to porcelain is acceptable and distortion during porcelain firing is very low [6-7]. Due to high yield strength of Co-Cr alloy, plastic deformation and porcelain debonding is rare for this alloy [8]. Nonprecious gold color (NPG) alloy is another base metal alloy, which is introduced in recent years to overcome Ni-Cr alloys limitations. It has surface characteristic of precious type III yellow gold. The manufactures claim that it can be used for full cast crowns, onlays, short span multiple unit bridges, metal substructure for veneer crowns using polymer resins, and post cores [9]. Khaledi et al. [10] showed that endodontically treated teeth that were restored with NPG posts, had higher fracture resistance than those with Ni-Cr posts. They attributed this property to similarity of elastic modulus of NPG posts and dentin structure, which was confirmed by later studies [11].

Having an acceptable castability is considered as one factor for accepting an alloy in dentistry. Castability is defined as the ability of a molten metal to completely fill the mold created by the burn out of wax pattern [12-13]. Many factors influence castability of an alloy. For example, type of alloy, wax pattern design, investment ingredients, burnout temperature, casting technique and direction of casting forces [14-17]. Casting of alloys might be done, using two types of casting machines; torch/centrifugal or induction/vacuum-pressure [18].

There is limited information available regarding castability of NPG alloy and Co-Cr alloy, using different casting techniques. Therefore, the purpose of this study was to compare the castability of Ni-Cr, NPG and Co-Cr alloys, using torch/centrifugal casting machine and induction/vacuum-pressure casting machine. The null hypothesis was that the castability of a dental alloy is not affected by the alloy type and casting machine.

**Materials and Method**

Castability of the tested alloys in this study follows the standard method of castability, proposed by Whitlock and Hinman in which the ability of an alloy to occupy a mold, which is created by burning out a mesh of nylon, is determined as castability standard test [19]. A total of 36 Wax patterns were prepared from a wax mesh pattern to design partial denture framework (Dandiran, Iran). The dimensions of each mesh were a square of 11mm*11mm with 16 square shaped spaces of 2mm*2mm and filament diameter of 1mm. Two runner bars of 10 gauges (Renfert, Germany) were attached to the two adjacent sides of each mesh. Then a 6-gauge sprue (Renfert, Germany) with the length of 10mm was attached to one corner of the mesh (Figure 1).

The pattern was attached to the crucible former and sprayed with a surface reducing agent (Lubrofilm, Den-taurum, Germany) and then air dried. Next, the pattern was invested with phosphate bonded investment (Bel-lasun, Bego) following the manufacturer’s instructions. The wax pattern was left to bench set for 60 minutes. Then, wax burn out was done by keeping the casting ring in the furnace (Magma, Renfert, Germany) and the temperature was raised to 250°C. This temperature was maintained for 1 hour. The temperature was raised further to 950°C and maintained for 1 hour in order to burn out the wax completely. In this stage, 36 mold cavities were created.

In the present study, three types of alloy were used for casting including Ni-Cr alloy (4all, Ivoclar Vivadent, Germany), Co-Cr alloy (MESA, Italy), and NPG alloy (AalbaDent, USA). Their chemical composition and properties are described in Table 1. Two casting techniques were performed in the current study including torch/centrifugal casting machine (Centrifii- co; Kerr Manufacturing) and induction/ vacuum-pressure casting machine (Nautilus t, Bego, Germany). Each alloy was casted, using both of these casting techniques. Therefore, six groups of alloys and casting techniques were created presented in Table 2. The casting of the created
molds was performed, using each alloy and a casting technique. Casting rings were bench cooled and then divested. Cleaning of the remaining investment was done with aid of ultrasonic and sandblasting with 50 to 70µm alumina particles (Hi-Aluminas, Shofu, Kyoto, Japan) (Figure 2).

The Castability value was calculated as described. The wax mesh with 16 square spaces provides 40 segments. The numbers of complete cast segments were counted, and castability value was calculated according to Whitlock suggested equation as follows:

\[
\text{Castability value} = \frac{\text{Number of completely cast segments}}{40} \times 100
\]

The effects of alloy type and casting method on product castability were then investigated statistically, using two-way ANOVA. The significance level was set at α=0.05.

### Results

The means and standard deviations of castability value for each group are shown in Table 3. In order to compare the means for each of the study group, Two-way ANOVA test and Tukey HSD tests were used. Two-way ANOVA test revealed no statistically significant interaction between the effects of alloy type and casting technique on castability value (F=1.286, p= 0.286). In addition, it represented no significant differences of castability regarding alloy type and casting technique with a p Value of 0.108 and 0.516, respectively.

### Table 3: Mean percentage castability values of three alloys, using two different casting methods

<table>
<thead>
<tr>
<th>Metal</th>
<th>Method</th>
<th>Mean</th>
<th>Std. Deviation</th>
<th>No.</th>
</tr>
</thead>
<tbody>
<tr>
<td>Ni-Cr</td>
<td>Induction</td>
<td>99.16</td>
<td>1.25</td>
<td>9</td>
</tr>
<tr>
<td></td>
<td>Centrifugal</td>
<td>98.61</td>
<td>2.2</td>
<td>9</td>
</tr>
<tr>
<td></td>
<td>Total</td>
<td>99.88</td>
<td>1.76</td>
<td>18</td>
</tr>
<tr>
<td>Co-Cr</td>
<td>Induction</td>
<td>99.72</td>
<td>0.83</td>
<td>9</td>
</tr>
<tr>
<td></td>
<td>Centrifugal</td>
<td>100</td>
<td>0</td>
<td>9</td>
</tr>
<tr>
<td></td>
<td>Total</td>
<td>99.86</td>
<td>1.06</td>
<td>18</td>
</tr>
<tr>
<td>NPG</td>
<td>Induction</td>
<td>99.44</td>
<td>1.66</td>
<td>9</td>
</tr>
<tr>
<td></td>
<td>Centrifugal</td>
<td>99.21</td>
<td>1.59</td>
<td>9</td>
</tr>
<tr>
<td></td>
<td>Total</td>
<td>98.88</td>
<td>1.9</td>
<td>18</td>
</tr>
</tbody>
</table>

### Table 4: Comparing castability values within groups

<table>
<thead>
<tr>
<th>Groups Compared</th>
<th>p Value</th>
<th>Significance</th>
</tr>
</thead>
<tbody>
<tr>
<td>A and B</td>
<td>0.97</td>
<td>No</td>
</tr>
<tr>
<td>A and C</td>
<td>0.97</td>
<td>No</td>
</tr>
<tr>
<td>A and D</td>
<td>0.86</td>
<td>No</td>
</tr>
<tr>
<td>A and E</td>
<td>0.86</td>
<td>No</td>
</tr>
<tr>
<td>A and F</td>
<td>0.99</td>
<td>No</td>
</tr>
<tr>
<td>B and C</td>
<td>0.65</td>
<td>No</td>
</tr>
<tr>
<td>B and D</td>
<td>0.42</td>
<td>No</td>
</tr>
<tr>
<td>B and E</td>
<td>0.99</td>
<td>No</td>
</tr>
<tr>
<td>B and F</td>
<td>0.86</td>
<td>No</td>
</tr>
<tr>
<td>C and D</td>
<td>0.68</td>
<td>No</td>
</tr>
<tr>
<td>C and E</td>
<td>0.99</td>
<td>No</td>
</tr>
<tr>
<td>C and F</td>
<td>0.97</td>
<td>No</td>
</tr>
<tr>
<td>D and E</td>
<td>0.22</td>
<td>No</td>
</tr>
<tr>
<td>D and F</td>
<td>0.65</td>
<td>No</td>
</tr>
<tr>
<td>E and F</td>
<td>0.65</td>
<td>No</td>
</tr>
</tbody>
</table>
The results of pairwise comparisons of castability values by using Tukey HSD are shown in Table 4.

Discussion
In this study, the castability value of Ni-Cr, Co-Cr and NPG alloys were tested, using both centrifugal and induction casting techniques. The results showed that there was no difference in the castability of these three types of alloys, using each casting technique, and therefore, the null hypothesis was accepted.

Due to increased cost of precious alloys, they are substituted by base metal alloys in dentistry. Ni-Cr is a base metal alloy which is mainly used to construct metal ceramic and cast post restorations [2]. Some countries replaced Ni-Cr alloy with Co-Cr alloy to restrict Ni allergen effects [3]. NPG alloy is another alloy which was introduced several years ago, with favorable characteristics [9].

Whitlock’s method was used in the present study to measure castability value of Ni-Cr, Co-Cr, and NPG alloys. The castability value of various alloys and casting techniques were measured using different methods [20]. However, it was found that Whitlock’s method is easy and does not require any special equipment to assess the castability. Furthermore, the size and the shape of each specimen can be easily standardized [19]. In this method, the number of completely casted segments is divided by total number of segments of the nylon mesh. Since the nylon mesh with the required dimensions was not available, Whitlock’s method was followed with a minor modification, which was the use of acrylic-wax mesh instead of polyester sieve cloth [21].

The mean castability values (in percentage) of the three alloys in the present study casted by using centrifugal and induction procedures were between 98.88% and 99.88%. The mean castability value of the tested alloys was close to ideal value of castability. Palaskar et al. [22] and Sharma et al. [23] evaluated the effect of recasting of Ni-Cr alloy, using the induction technique. The mean castability value of new alloy in these studies was 99.36% in the first study and 100% in the second study. The castability value of Ni-Cr alloy by induction method in the current study was 99.88%, which was in line with the mentioned studies.

Imran et al. [24] evaluated the effect of reused Co-Cr alloy on its castability value, using torch centrifugal method. Their result showed no significant difference of castability value amongst the tested groups. The mean castability value of new alloy was 100% in this study. These results are in agreement with the present study, where the mean castability value of Co-Cr in centrifugal method was 100%.

Carreiro et al. [25] compared the castability of Ni-Cr and Co-Cr alloys (Remanium 2000) which is mainly used for the framework of metal ceramic restorations and found that the castability of Remanium 2000 was less than the Ni-Cr. This finding is in contrast with present study, which might be due to different composition of tested alloys. The Co-Cr alloy in the present study consisted of Co (64%), Cr (21%), Molybdenium (6%), vanadium (6%), Si, Fe, and Mn. However, Carreiro et al. used Co (61%), Cr (25%), Molybdenium (5%), vanadium (1.5%) and Si composition.

A study by Thompson et al. [26] evaluated the effect of both torch/centrifugal and induction/vacuum-pressure casting machines on the castability of four dental casting alloys (Genesis II, Liberty, Olympia, Jelenko O). Genesis II is a nickel-free cobalt-chromium-molybdenum base metal alloy, and found no difference in the castability of Genesis II, using the two casting techniques, which is compatible with the results of the current study. However, the castability index between Genesis II and Olympia (gold-palladium high noble alloy) was different, which could be related to different alloy ingredients [26].

The difference between the castabilities of alloys might be related to several items, such as composition, density, surface tension, fluidity and permeability of the alloy, casting pressure, casting method, investment composition, the mold temperature, and melting atmosphere [27]. One of the limitations of this study was that the specimens were in the form of mesh and not the actual restoration. However, the method to measure castability of the actual form of mesh and not the actual restoration. Further studies should be carried out to investigate the physical properties of Co-Cr and NPG alloys, using different casting techniques.

Conclusion
Within the limitations of this study, it can be concluded that no significant difference was found in the castability value of Ni-Cr, Co-Cr, and NPG alloys. Also, the
castability value of the three tested alloys in this study was not different when using torch/centrifugal and induction/vacuum-pressure casting machines.

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Conflict of Interest
The authors declare that they have no conflict of interest.

References


